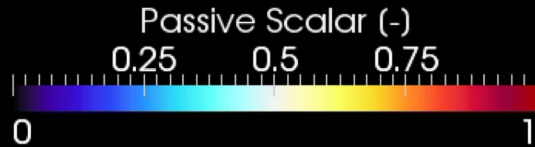


# Towards optimization of reactive flows in SU2

Time: 0.0000 s



RTC5.2

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(Bosch Research & Technology Center, Sunnyvale)

# Bosch – Overview

## Corporate Research – RTC-NA



### America

Research and Technology Center North America

**130 associates**

### Europe

- ▶ Corporate Research Germany
- ▶ Research and Technology Office Russia
- ▶ Research and Technology Office Tel Aviv

**1,400 associates**

### Asia-Pacific

- ▶ Research and Technology Center India
- ▶ Research and Technology Center Asia-Pacific

**110 associates**

# Bosch – Overview

## Thermotechnology – Residential Heating



402,166

Bosch associates make  
these solutions possible



60 countries

–  
440 regional  
subsidiaries

### Four business sectors



Mobility  
Solutions



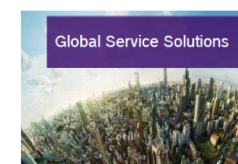
Industrial  
Technology



Energy & Building  
Technology

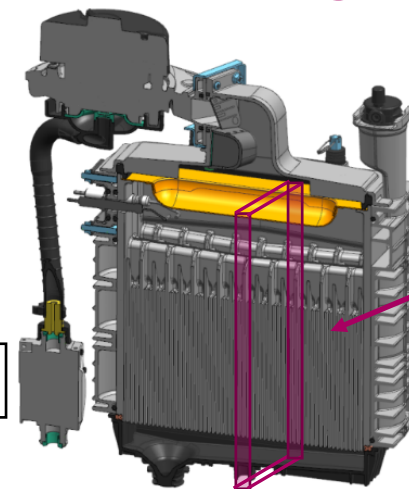
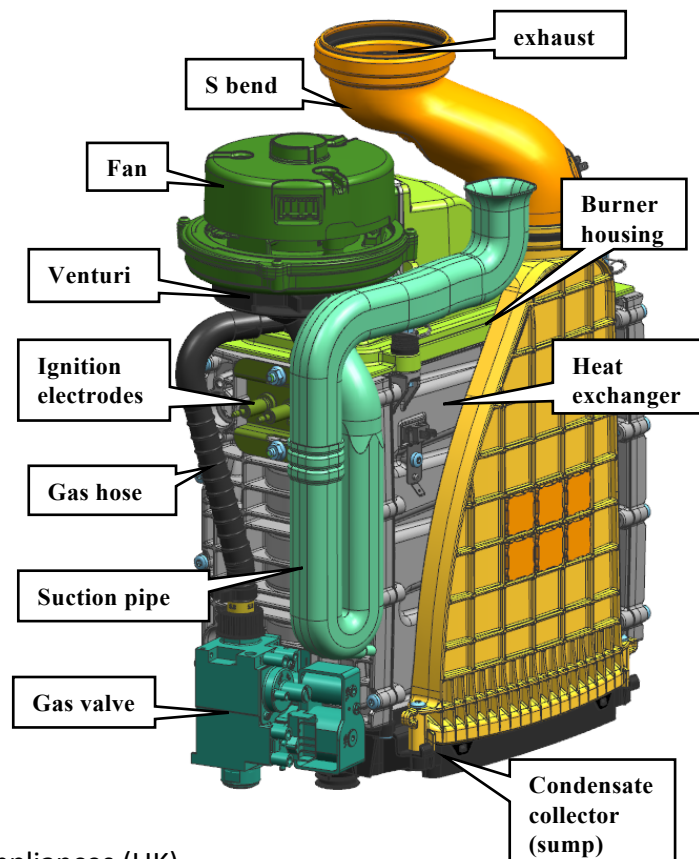


Consumer  
Goods

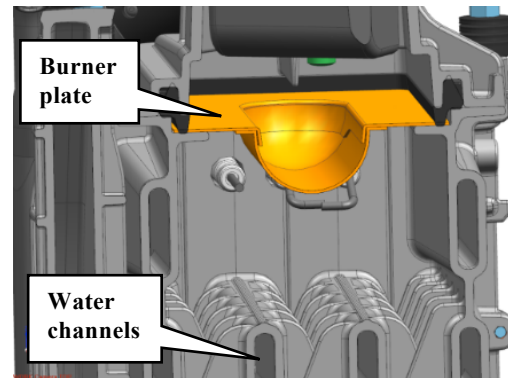


# Bosch Thermotechnology – Residential Heating

## Domestic wall mounted boiler with WB7 heat exchanger



A slice of the heat exchanger is simulated to assess performance and improve design



- WB7 Heat exchanger (7-37 kW)
- Used in Trendline (NL) and Greenstar appliances (UK)

We want a good estimate of emissions ( $\text{CO}$ ,  $\text{NO}_x$ ) in early stages of development

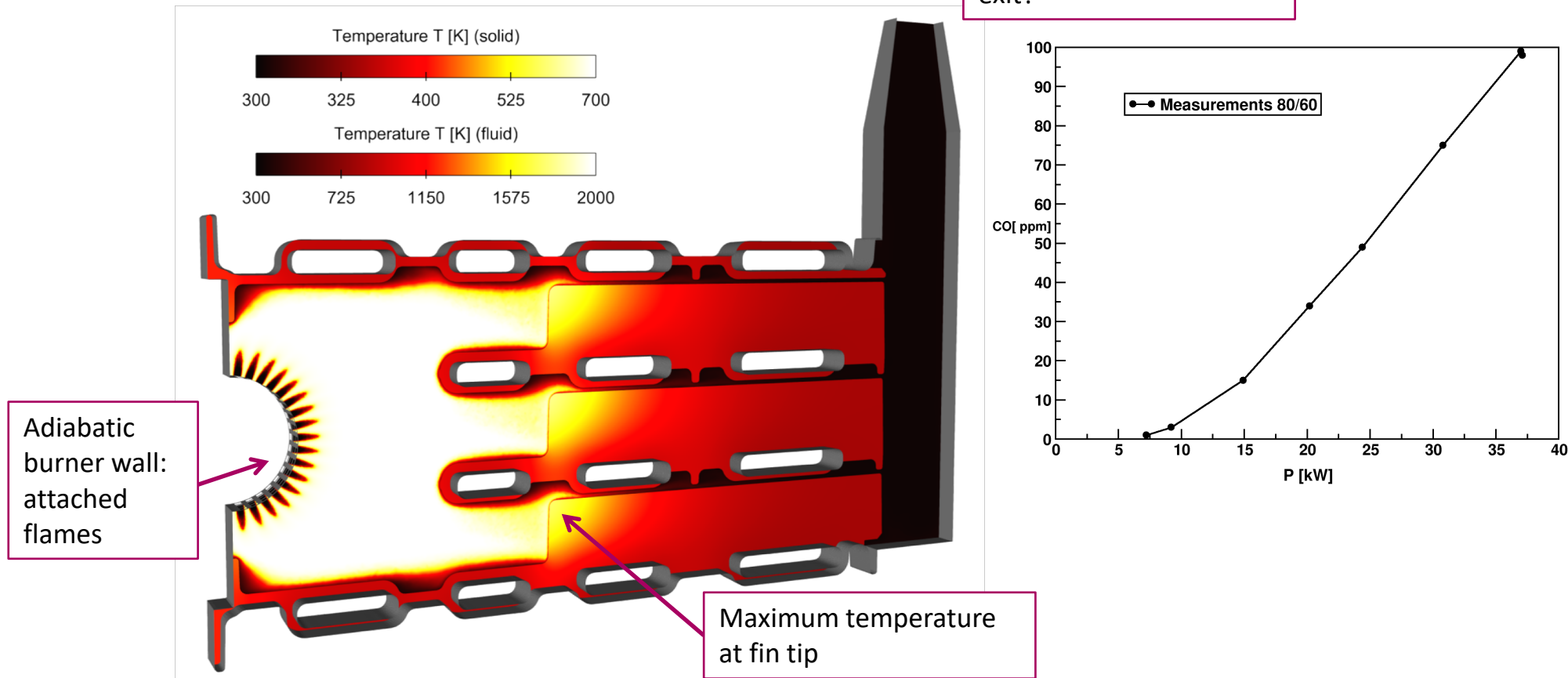


# Prediction and reduction of emissions in domestic boilers

## How much CO, NO<sub>x</sub> is produced?



How much CO at the exit?



We want a good estimate of emissions (CO, NO<sub>x</sub>) in early stages of development

# Prediction and reduction of emissions in domestic boilers

## For combustion simulations we need the chemical reactions

Detailed description of methane-air combustion consists of many reactions involving many species being produced during the reaction, e.g. The GRI-3.0 mechanism from Berkeley:

**53 SPECIES:** H2 H O O2 OH H2O HO2 H2O2 C CH CH2 CH2(S) CH3 CH4 CO CO2 HCO CH2O  
CH2OH CH3O CH3OH C2H C2H2 C2H3 C2H4 C2H5 C2H6 HCCO CH2CO HCCOH N NH NH2 NH3  
NNH NO NO2 N2O HNO CN HCN H2CN HCNN HCNO HOCN HNCO NCO N2 AR C3H7 C3H8  
CH2CHO CH3CHO

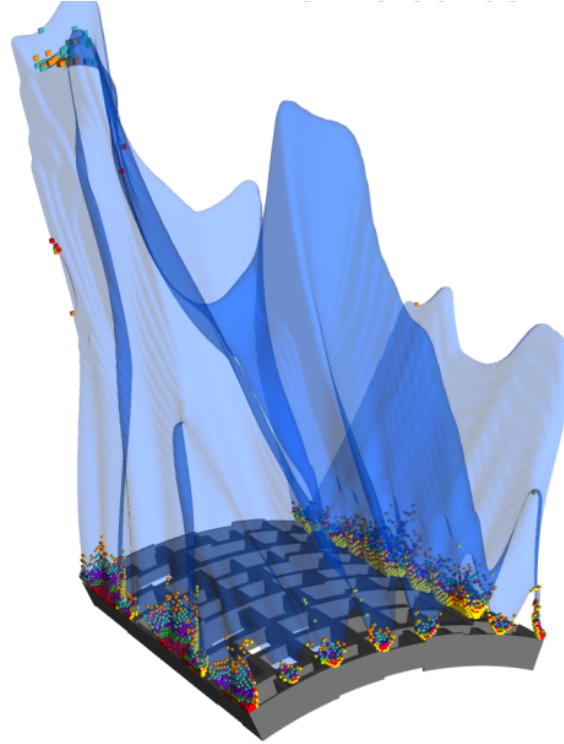
### ► 325 reactions:

- (1)  $O + H_2 \rightleftharpoons H + OH$
- (2)  $O + HO_2 \rightleftharpoons OH + O_2$
- (3)  $O + H_2O_2 \rightleftharpoons OH + HO_2$
- ...
- (325)  $CH_3 + C_3H_7 \rightleftharpoons 2C_2H_5$

Solving 53 transport equations for the species is too expensive for industrial 3D CFD simulations

# Prediction and reduction of emissions in domestic boilers

## General idea of flamelets: observation

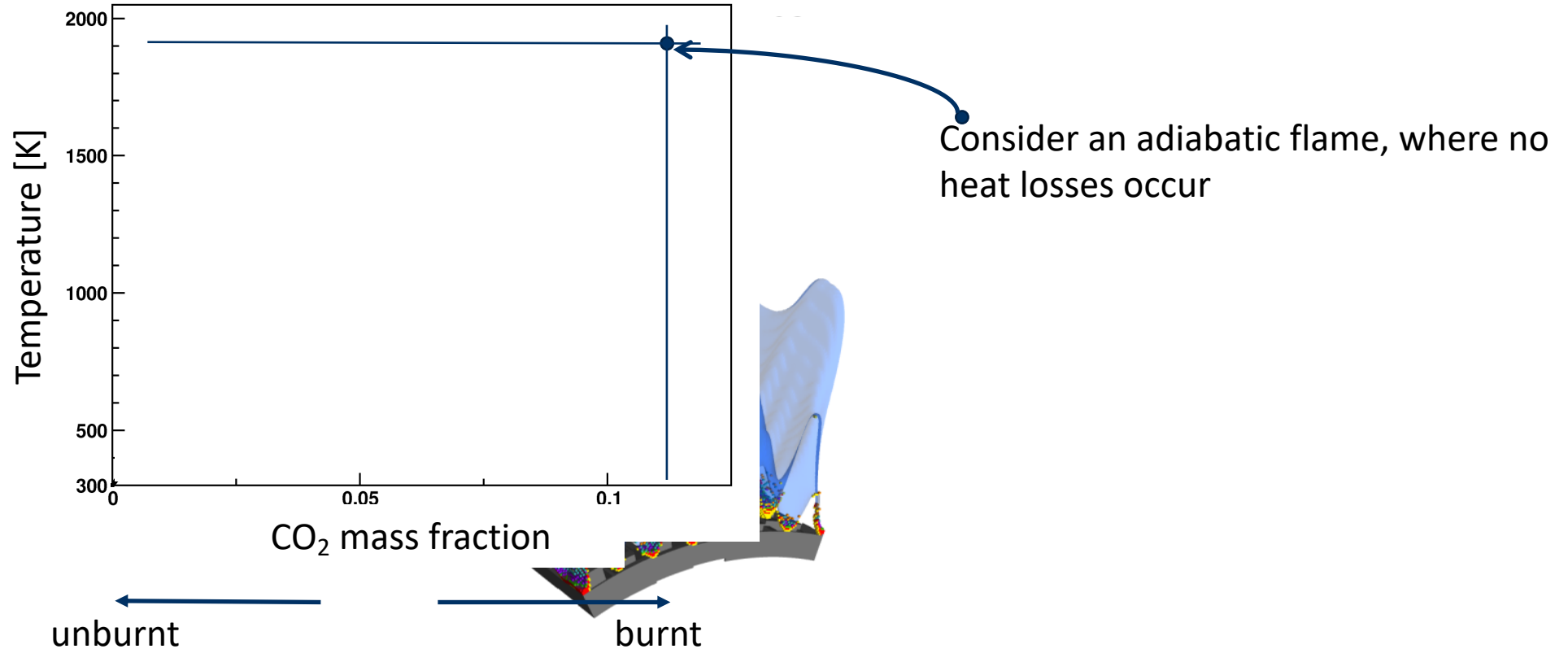


Consider an adiabatic flame, where no heat losses occur

Flame properties (temperature, concentrations) are complex structures in 3D

# Prediction and reduction of emissions in domestic boilers

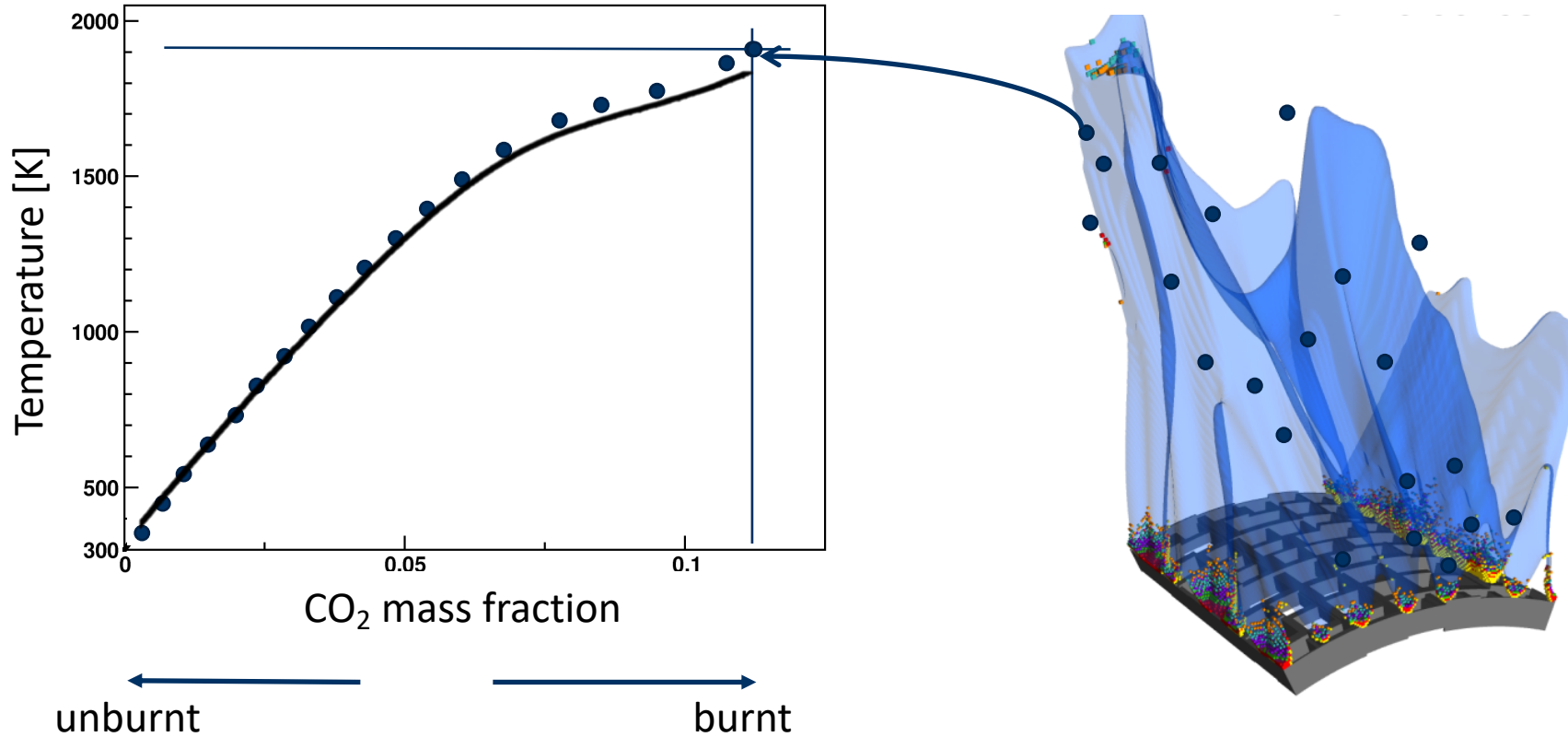
## General idea of flamelets: observation



Plot temperature etc. as function of a combustion progress variable, e.g. CO<sub>2</sub>

# Prediction and reduction of emissions in domestic boilers

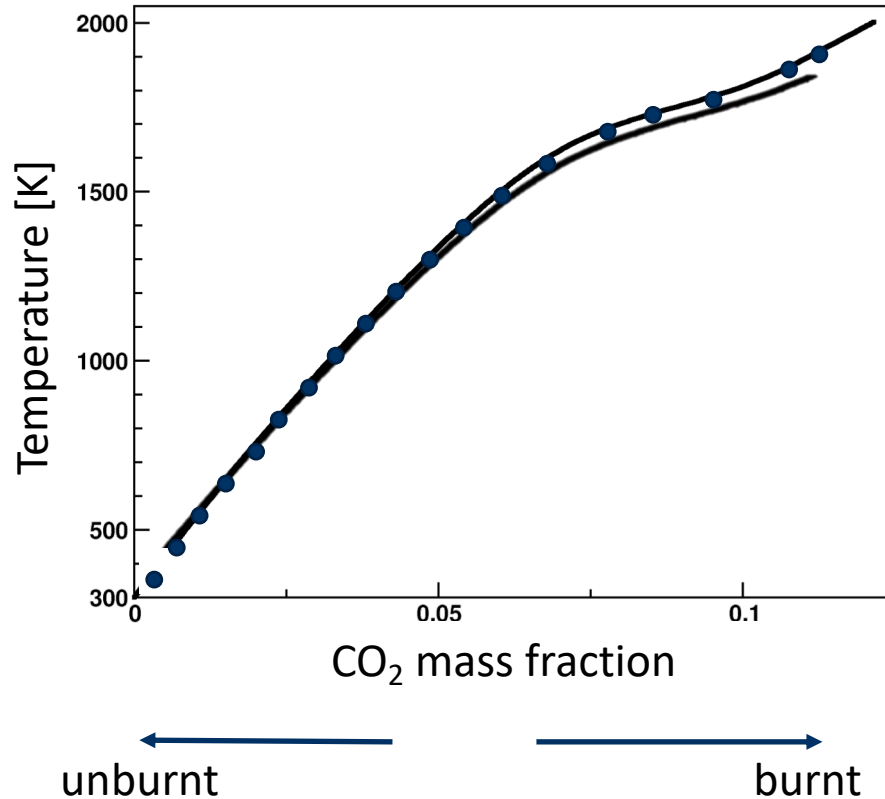
## General idea of flamelets: observation



All points fall on a single line: flames are one-dimensional in progress variable space

# Prediction and reduction of emissions in domestic boilers

## General idea of flamelets: observation



Enthalpy is constant in adiabatic flame

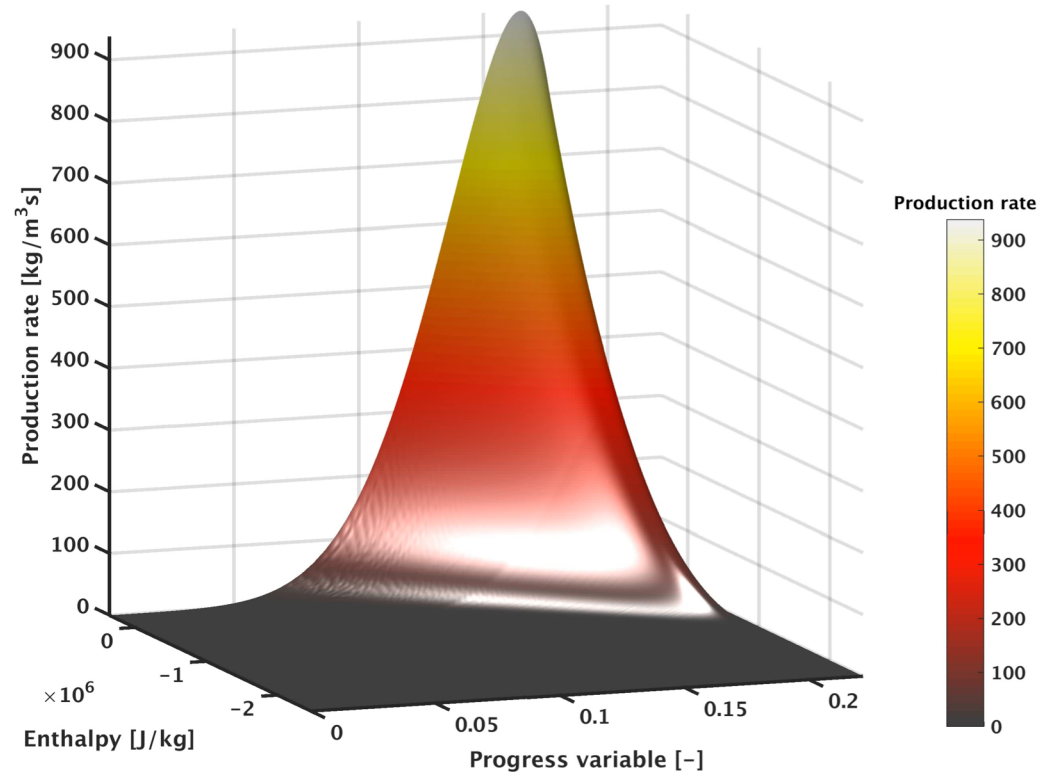
Enthalpy decreases if e.g. the inlet temperature is decreased

This can be used in simulations with heat losses

The lines compose a unique 2D flamelet generated manifold in progress variable-enthalpy space

# Prediction and reduction of emissions in domestic boilers

## Flamelet modelling of combustion



- Solve transport equation for progress variable and enthalpy:

$$\frac{\partial(\rho C)}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v} C) - \vec{\nabla} \cdot (\rho \mathcal{D}_C \vec{\nabla} C) = \rho \dot{\omega}_C$$

$$\frac{\partial(\rho h)}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v} h) - \vec{\nabla} \cdot (\rho \mathcal{D}_h \vec{\nabla} h) = 0$$

- Retrieve production rate (source term) from FGM lookup table
- Retrieve temperature, density, viscosity etc. from FGM lookup table



# Implementation models in SU2

## General idea of implementation (in progress)

- General framework for solving system of transport equations of species:

$$\frac{\partial \rho y_i}{\partial t} + \nabla \cdot (\rho u y_i) = \nabla \cdot (\rho D_i \nabla y_i) + S$$

- Specific implementations for species transport, non-premixed and premixed combustion, as well as finite rate chemistry:

$$\text{e.g. } S_{\text{prem}} = \rho_u S_L \nabla |c|$$

- Fluid properties from
  - Built-in functions (for simple problems, e.g. constant properties per species, implementation of mixing rules)
  - Lookup tables (for combustion)
  - External library (e.g. mutation++ or fluidprop)

# SU2 - scalar transport

## Transport equation for a scalar has been added

### Example 1: transported scalar

```
%scalar transport. Options: PASSIVE_SCALAR, PROGRESS_VARIABLE
KIND_SCALAR_MODEL= PASSIVE_SCALAR

% mass diffusivity. Options: CONSTANT_DIFFUSIVITY, CONSTANT_SCHMIDT
DIFFUSIVITY_MODEL=CONSTANT_DIFFUSIVITY
DIFFUSIVITY_CONSTANT= 0.002

% write diffusivity to file
WRT_DIFFUSIVITY=yes

% initialization of the domain
SCALAR_INIT=0.0

% in case of turbulence we need the turbulent Schmidt number
%SCHMIDT_TURB=0.7

% scalar clipping
SCALAR_CLIPPING= YES
SCALAR_CLIPPING_MIN= 0.0
SCALAR_CLIPPING_MAX= 1.0
```

### Example 2: premixed combustion

```
% scalar transport. Options: PASSIVE_SCALAR, PROGRESS_VARIABLE
KIND_SCALAR_MODEL= PROGRESS_VARIABLE

% laminar flamespeed for premixed combustion [m/s]
PREMIXED_LAMINAR_FLAMESPEED= 0.5

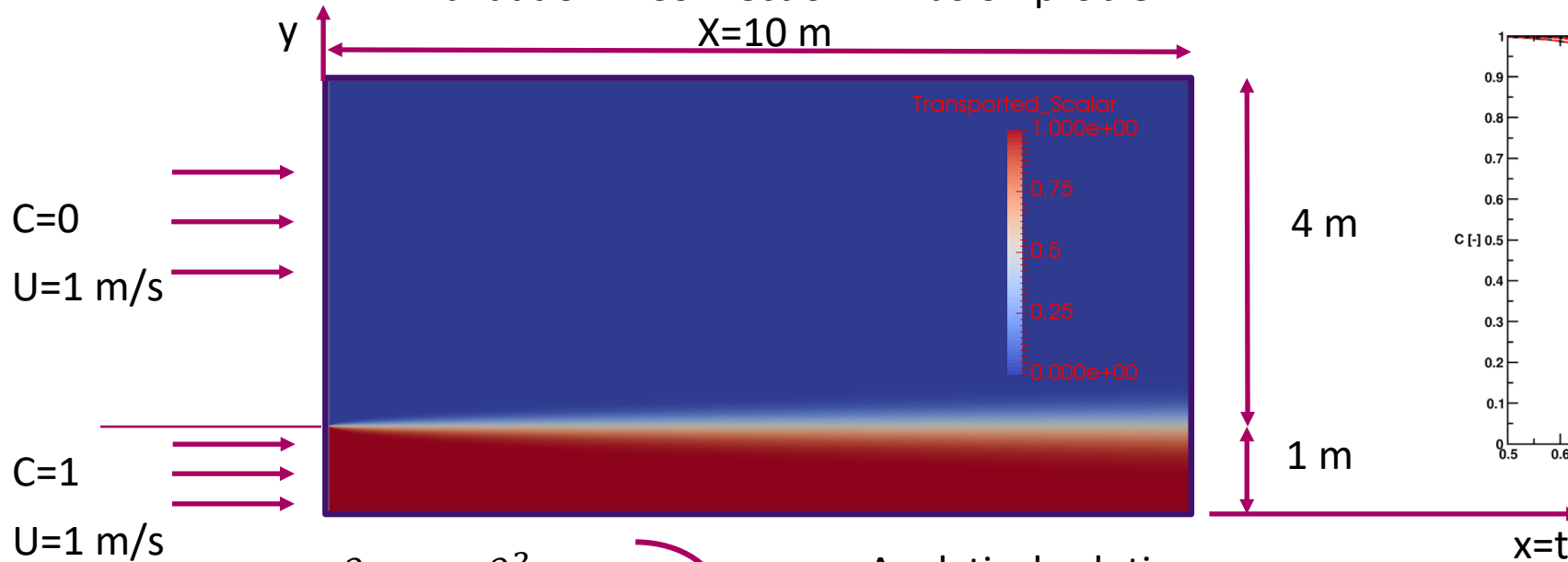
% adiabatic flame temperature for premixed combustion
% note that unburnt temperature comes from reference values
PREMIXED_FLAME_TEMPERATURE= 1800
```

# VALIDATION

# SU2 – passive scalar transport

## Scalar transport equation has been added to SU2

Validation 1: Convection-Diffusion problem



$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial y^2}$$

Boundary condition:

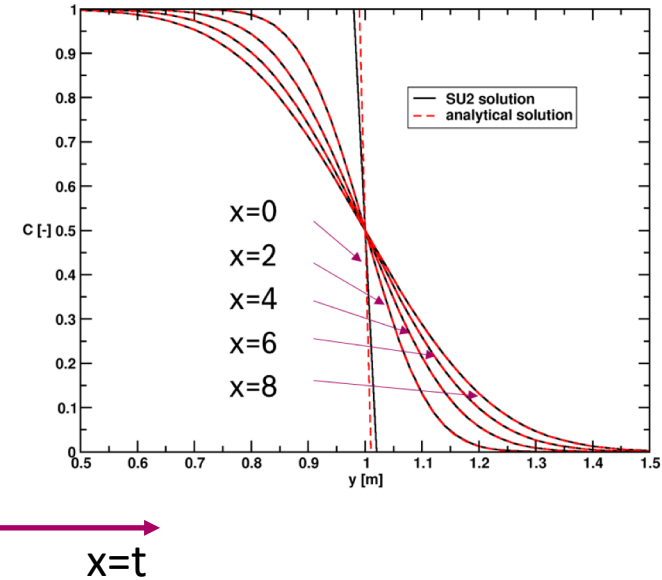
$$C(y < 1, 0) = 1$$

$$C(y > 1, 0) = 0$$

Analytical solution:

$$c(y, t) = \frac{1}{2} \left( 1 + \operatorname{erf} \left( \frac{y}{\sqrt{4Dt}} \right) \right)$$

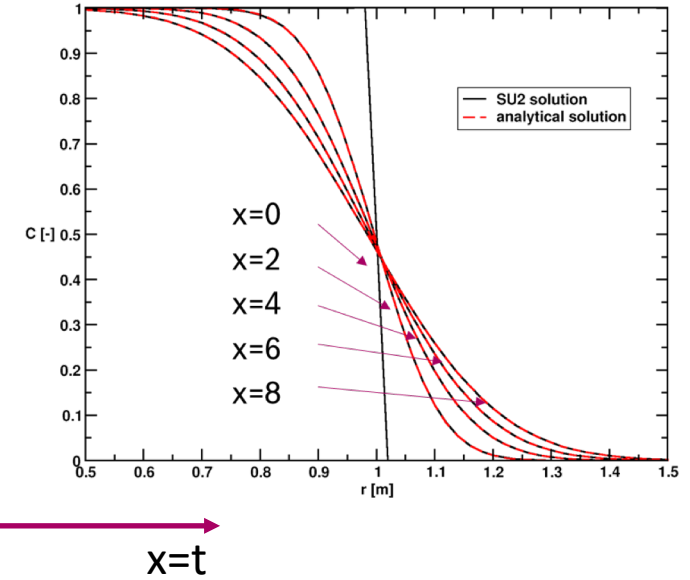
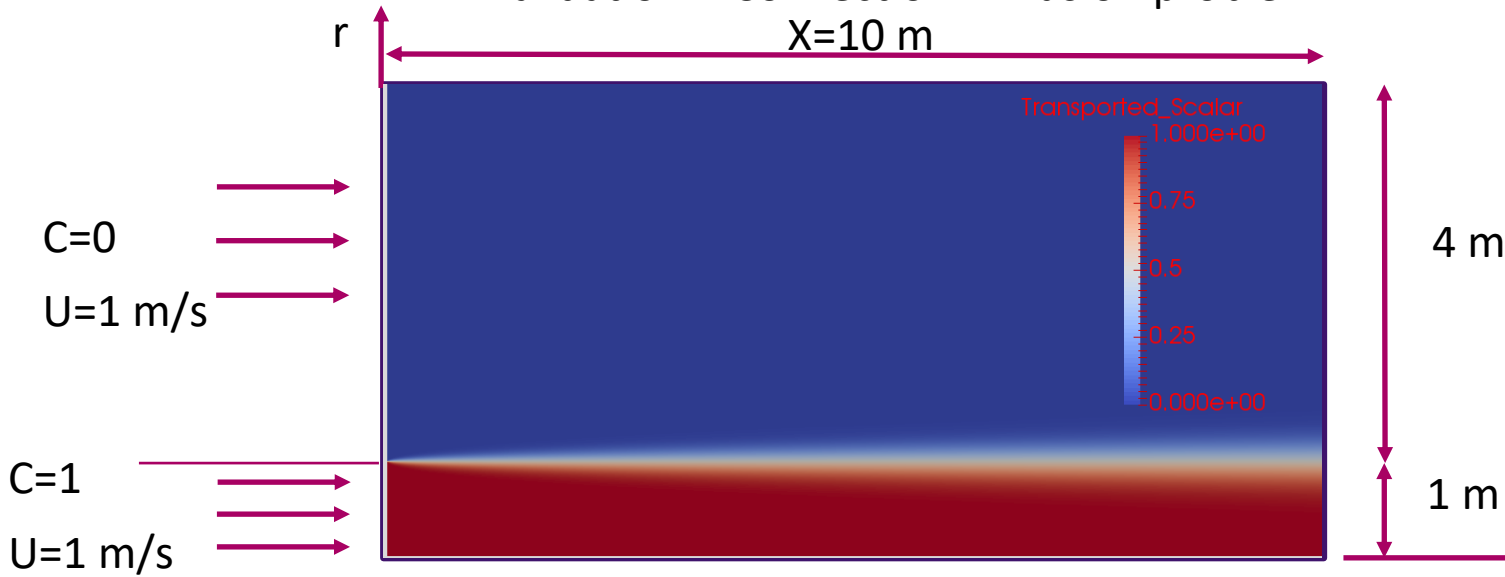
$$D = 0.02$$



# SU2 – passive scalar transport

## Axisymmetric case

Validation 2: Convection-Diffusion problem  
X=10 m



$$\frac{\partial c}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left( D r \frac{\partial c}{\partial r} \right)$$

Boundary condition:  $c(r,0)=f(r)$

$c(r,0)=1, r<1$

$c(r,0)=0, r>1$

Analytical solution:

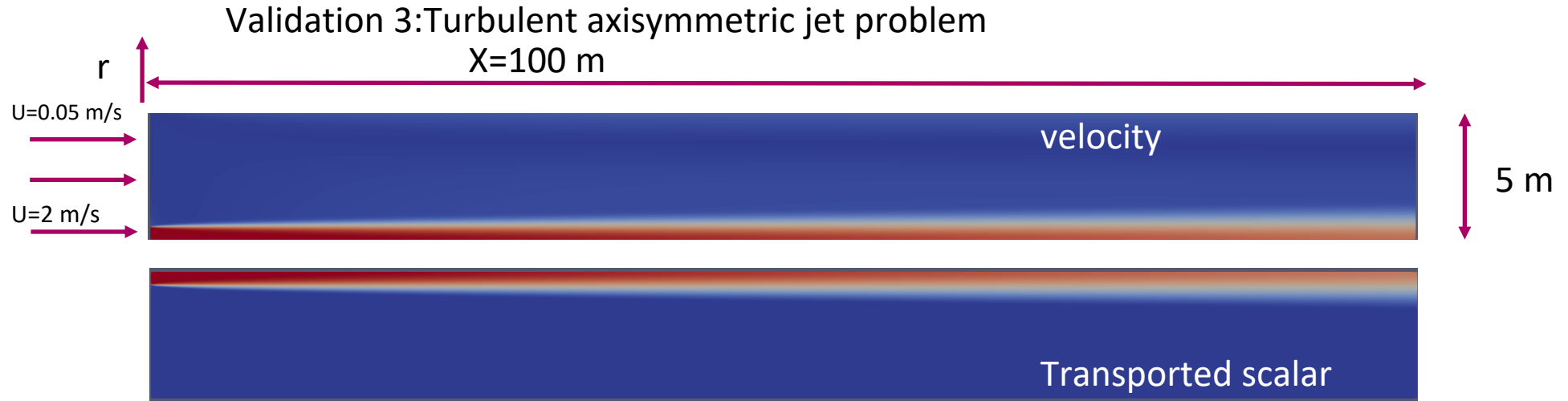
$$c(r, t) = \frac{2}{R^2} \sum_{n=1}^{\infty} e^{-D\alpha_n^2 t} \frac{J_0(r\alpha_n)}{J_1(R\alpha_n)} \int_0^R r f(r) J_0(r\alpha_n) dr$$

$D=0.02, R=5,$

$\alpha_n$  are roots of  $J_0(R\alpha_n)$

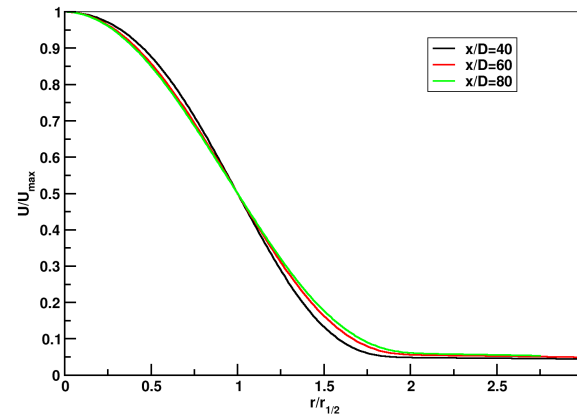
# SU2 – passive scalar transport

## Turbulent jet with SA turbulence model



### Validation:

- Velocity and scalar should be self-similar downstream
- Other validation: spreading rate ( $\sim 0.11$ ), measurements (e.g. Wygnanski & Fiedler)
- Note that SA is known to perform badly for round jet



## SU2 - scalar transport

### Laminar premixed flame with laminar flamespeed model

The mean reaction rate of a premixed flame can be modelled as:

$$S = \rho_u S_L \frac{A_T}{A} |\nabla c|$$

In turbulent flames, the flame wrinkling is nonunity:

$$\frac{A_T}{A} = 1 + \frac{0.46}{Le} Re_t \frac{u'^{0.3}}{S_L} \frac{p^{0.2}}{p_0}$$

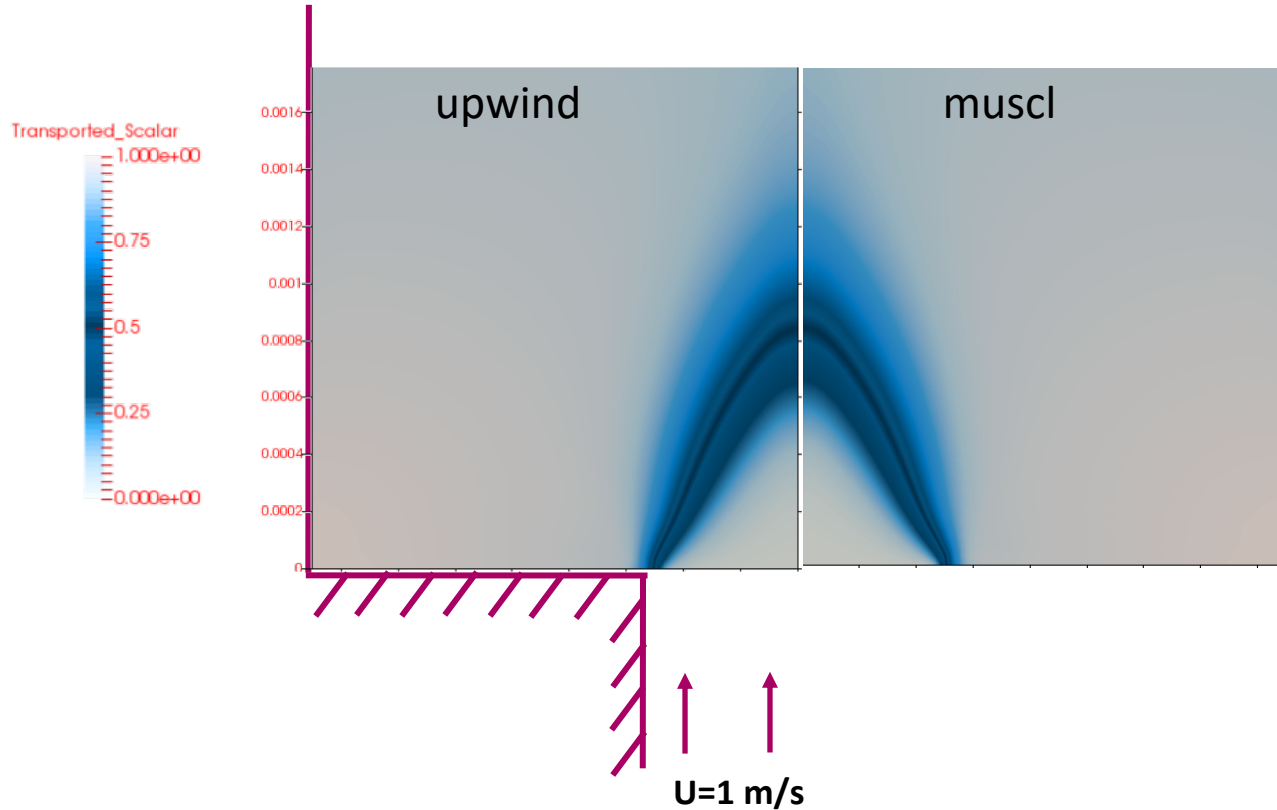
Temperature is linear function of progress variable:

$$T = T_u \cdot (1 - c) + T_f \cdot c$$



# SU2 - scalar transport

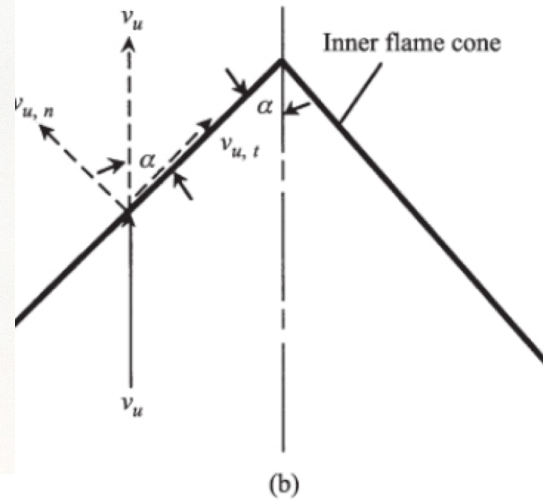
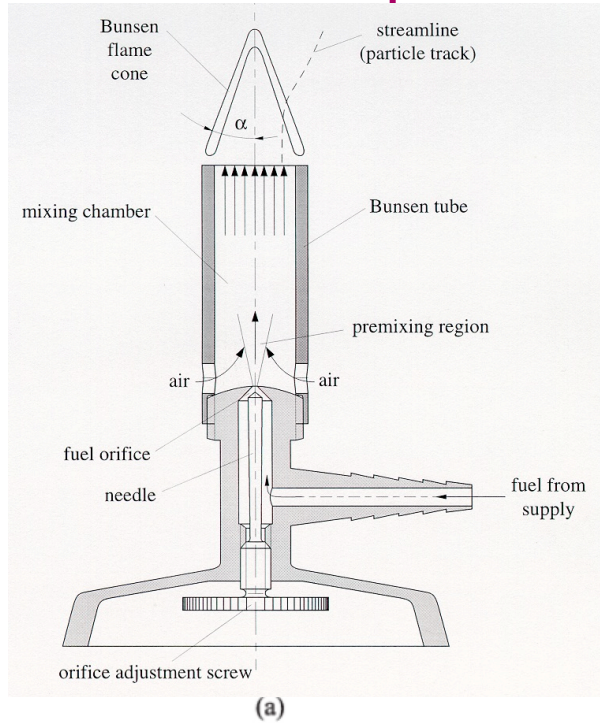
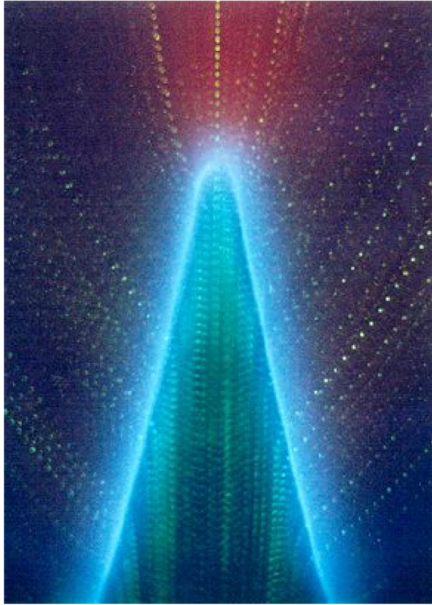
## Planar laminar premixed flame



- A premixed 'no-chemistry' flame simulation is possible now in SU2
- Temperature is a function of progress variable:  $T=T(c)$
- Density is multicomponent ideal gas law  $\rho = \rho(T, c)$
- Currently, other properties like viscosity not coupled directly
- Convergence is not so good yet

# Outlook: Adjoint optimization of Bunsen burner

## Determine laminar flame speed from flame angle



- Laminar flame speed determines flame shape (angle)
- For accurate measurements of flame speed a straight flame profile is necessary
- A uniform velocity profile is crucial
- Objective: optimization of uniformity of velocity profile at Bunsen tube exit

Bunsen Burner Methane-Air Premixed Flame

**Figure 8.3** (a) Bunsen-burner schematic. (b) Laminar flame speed equals normal component of unburned gas velocity,  $v_{u,n}$ .

$$S_L = v_{u,n} = v_u \sin \alpha$$

# Combustion models in SU2

## Final words

- Basic framework for transported scalars was implemented
- Work on lookup table approach will start soon (in collaboration with
- Besides implementing models, convergence needs attention
- Code is available on github in branch `feature_scalar`
- Looking forward to a good collaboration!



**SU2**  
The Open-Source CFD Code